

Department of Civil Engineering  
Kattahar Engineering College, Kattahar

Subject: Design of Concrete Structure-I

Topic: Column

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Lecture: 02

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# Design of Lateral Ties :

## ① Diameter

- Max<sup>n</sup> value
- (a)  $\frac{\phi_{main}}{4}$  [  $\phi_{main} = \text{Dia of main reinf}^n$  (larger dia) ]
  - (b) 6 mm

## ② Spacing

- Min<sup>m</sup> value
- (i) Least lateral dimension (say B)
  - (ii)  $16 \phi_{main}$  [  $\phi_{main} = \text{smaller dia of main reinforcement}$  ]
  - (iii) 300 mm

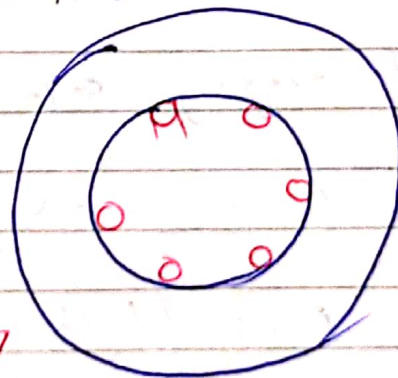
## # Design of circular column :

① Circular column WITH separate lateral ties  
For a long column

(a) load carrying capacity

$$P = C_r \cdot (\sigma_{sc} \cdot A_{sc} + \sigma_{cc} \cdot A_c)$$

$$P = \left( 1.25 - \frac{\text{Lfl}}{48D} \right) (\sigma_{sc} \cdot A_{sc} + \sigma_{cc} \cdot A_c)$$

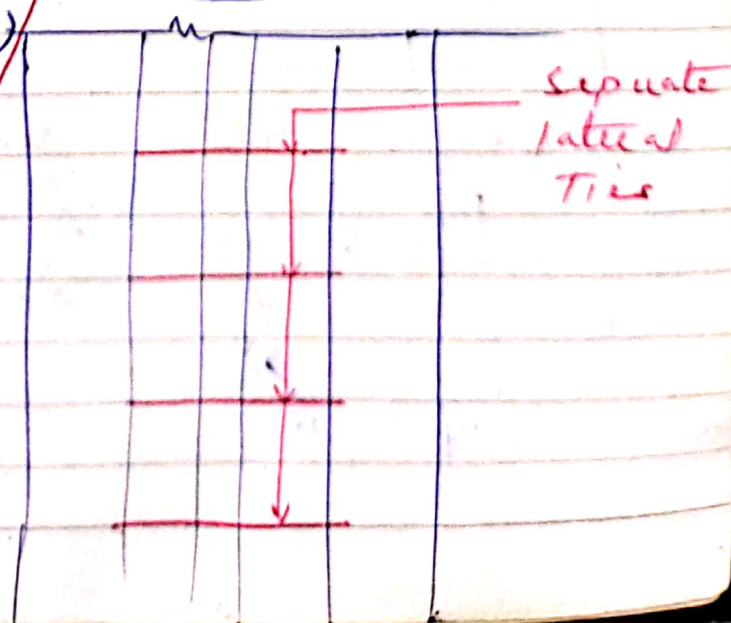


## ② Design of lateral ties

- ① Dia
- (a)  $\frac{\phi_{main}}{4}$  } Max<sup>m</sup>
  - (b) 6 mm

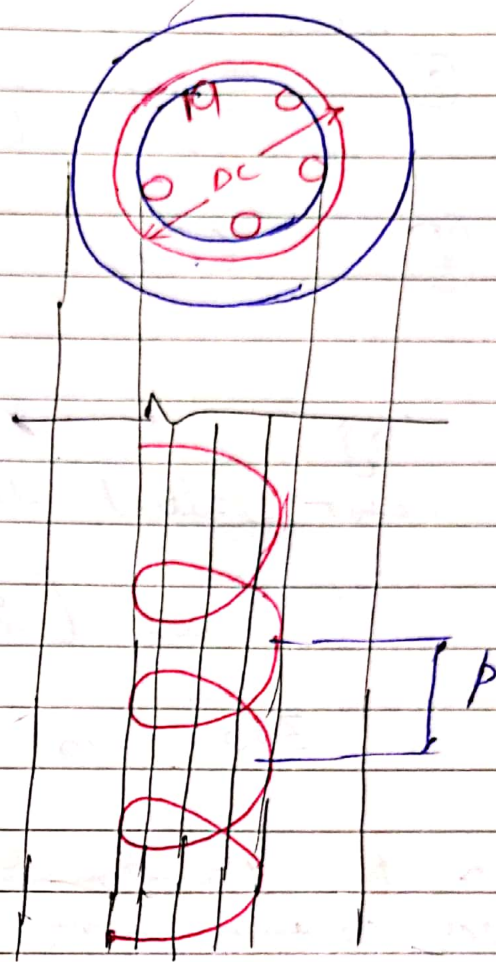
## ② Spacing

- (a) LLD
- (b) 16  $\phi$  (LL) 300 mm



② ~~Column~~ Circular column with helical reinforcement

→ Load carrying capacity is increased by 5%.



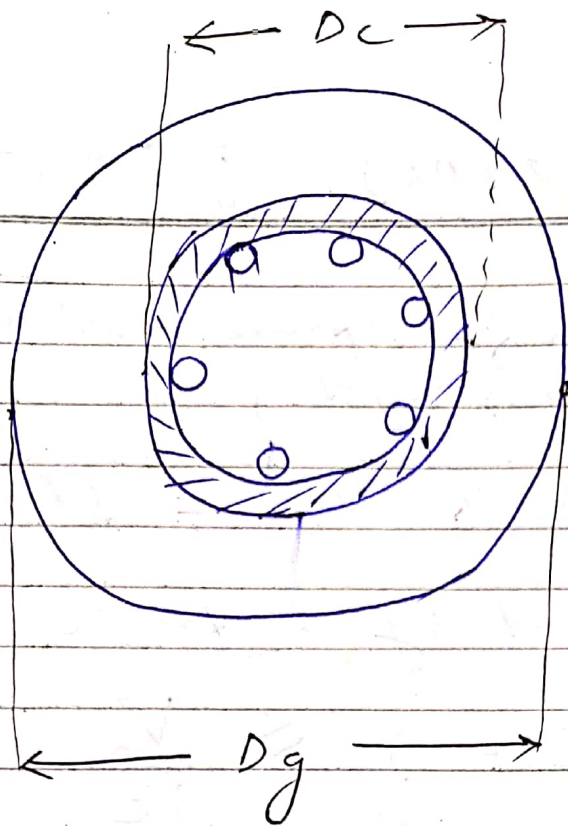
→ load carrying capacity of a long column

$$P = 1.05 \times C_r (\sigma_{sc} \cdot A_{sc} + \sigma_{cc} \cdot A_c)$$

$$P = 1.05 \times \left( 1.25 - \frac{L_{eff}}{48 D_c} \right) (\sigma_{sc} \cdot A_{sc} + \sigma_{cc} \cdot A_c)$$

→ Design of helical reinforcement

$$0.36 \frac{f_{ck}}{f_y} \left( \frac{A_g}{A_c} - 1 \right) \leq \frac{V_k}{V_c}$$



# ①  $A_g$

$D_g = D =$  Gross diameter

$$A_g = \frac{\pi}{4} \times (D_g)^2$$

②  $D_c$  (Core diameter)  
Outside to outside of helical reinforcement

$$D_c = \frac{D_g - 2 \times \text{clear cover}}{D_g - 2 \times 40}$$

$$A_c = \frac{\pi}{4} \times D_c^2$$

$V_c =$  Volume of core for unit length  
of column ( $1\text{m} = 1000\text{mm}$ )

$$V_c = A_c \times 1000\text{mm}^3$$

③  $V_h \rightarrow$  volume of helical reinforcement for unit  
length of column.

$$= (\text{No of turns}) \times (\text{length in one turn}) \times \left(\frac{C/S}{\text{dia}}\right)$$

$$V_h = \left( \frac{1000}{\rho} \right) \times (\pi \times D_h) \times \frac{\pi}{4} (\phi_h)^2$$

Where  $\pi D_h \rightarrow$  length of reinforcement in one full (approx length)

$$D_h \rightarrow \text{Dia of helix} = (D_c - \phi_h)$$

pitch can be found by the formula

$$0.36 \frac{f_{ck}}{f_y} \left( \frac{A_g}{A_c} - 1 \right) \leq \frac{V_h}{V_c}$$

pitch (p)

①  $p \neq 75 \text{ mm}$

②  $p \neq \left( \frac{D_c}{6} \right)$

③  $p \neq 25 \text{ mm}$

④  $p \neq 3 \phi_h$

As per

26.5.3.2 (d)

(P-49)

Pr 25.1.2 A compression member may be considered short if both  $\left( \frac{L_{ex}}{b} \right)$  or  $\left( \frac{L_{ey}}{B} \right) < 12$

Pr 25.2 Effective length of column.

Refer Table 28 / Annexure - E

Pr 25.3 Slenderness Limit

Unsupported length  $\neq 60 \times$  least lateral dimension

$$60B \text{ or } \left( \frac{100 B^2}{D} \right)$$

<Happy learning>