



**Department of Civil Engineering**  
**Katihar Engineering College, Katihar**

**Subject :** Soil & Rock Mechanics

**Topic :** Stability of Slopes (Infinite Slope)

**Lecture :** 02

**Course Instructor :** Prof. Rashid Mustafa

Case b . Submerged Slope : ( Cohesionless Soil )

$$\sigma_z = \gamma' z \cos \beta$$

$$\sigma_n = \gamma' z \cos^2 \beta$$

$$\tau = \gamma' z \cos \beta \cdot \sin \beta$$

$$\text{Shear strength} = \sigma_n \tan \phi = \gamma' z \cos^2 \beta \cdot \tan \phi$$

$$\text{Factor of safety (FOS)} = \frac{\tau_f}{\tau} = \frac{\gamma' z \cdot \cos^2 \beta \cdot \tan \phi}{\gamma' z \cos \beta \cdot \sin \beta}$$

$$\boxed{\text{FOS} = \frac{\tan \phi}{\tan \beta}}$$

→ FOS of dry / Moist Slope is same as that of submerged slope .

→ The change in depth of critical section causes change in value of Normal stress & shear stress acting on it. but ratio of the stresses remains constant

Case 3 . For  $c - \phi$  soil

(2)

$$FOS = \frac{\tau_f}{\tau} = \frac{c + \sigma_n \tan \phi}{\tau}$$

$$\sigma_n = \gamma z \cos^2 \beta .$$

$$\tau = \gamma z \cos \beta \cdot \sin \beta .$$

$$\text{Factor of Safety (FOS)} = \frac{c + \gamma z \cos^2 \beta \cdot \tan \phi}{\gamma z \cos \beta \cdot \sin \beta .}$$

↳ For  $c - \phi$  soil

Where  $c \rightarrow$  cohesion of the soil  
 $\gamma \rightarrow$  unit wt of soil  
 $\beta \rightarrow$  slope angle  
 $\phi \rightarrow$  Angle of internal friction -

Let  $H_c$  be the critical height of the slope (the height for which factor of safety is equal to one i.e.

$$FOS = 1 \quad (\tau_f = \tau)$$

$$1 = \frac{c + \gamma H_c \cos^2 \beta \cdot \tan \phi}{\gamma H_c \cos \beta \cdot \sin \beta .}$$

$$\gamma H_c \cos^2 \beta \cdot \sin \beta - \gamma H_c \cos^2 \beta \cdot \tan \phi = c \quad (3)$$

$$H_c = \frac{c}{\gamma \cos^2 \beta (\sin \beta - \cos \beta \cdot \tan \phi)}$$

$$H_c = \frac{c}{\gamma \cos^2 \beta (\tan \beta - \tan \phi)} \quad (2)$$

When  $H_c \rightarrow$  Critical height  
(FOS = 1 or  $\tau_f = \tau$ )

From (2)

$$\gamma H_c = \frac{c}{\cos^2 \beta (\tan \beta - \tan \phi)}$$

$$\frac{c}{\gamma \cdot H_c} = \cos^2 \beta (\tan \beta - \tan \phi)$$

When  $\frac{c}{\gamma H_c} = S_n =$  Dimensionless quantity  
known as stability  
number.

$$\text{Stability Number } (S_n) = \frac{c}{\gamma H_c} = \cos^2 \beta (\tan \beta - \tan \phi)$$

If a factor of safety  $F_c$  is applied to the cohesion such that mobilised cohesion at a depth  $H$ .

$$C_m = \frac{C}{FOS}$$

Where  $C_m \rightarrow$  Mobilised cohesion

$$S_n = \frac{C_m}{\gamma H} = \frac{C}{FOS \cdot \gamma \cdot H}$$

It can be also written as

$$S_n = \frac{C}{\gamma H c} = \frac{c}{F_c \cdot \gamma H}$$

$$F_c = \frac{Hc}{H}$$

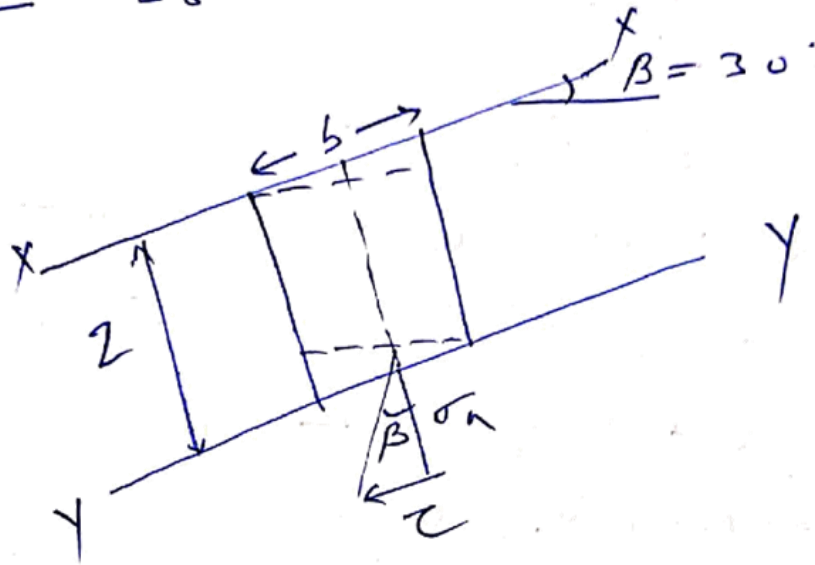
$$FOS = F_c = \frac{Hc}{H} = FH$$

Where  $F_c \rightarrow$  Factor of safety w.r.t cohesion

$FH \rightarrow$  Factor of safety w.r.t height.

P-1

A slope of infinite extent is made in a dense layer at an angle of  $30^\circ$  to the horizontal. Determine the factor of safety of the slope against shear failure if the angle of internal friction of the soil to be  $36^\circ$ .



$$\begin{aligned} \text{Vertical stress on } Y-Y &= \sigma_z \cos \beta \\ &= (\gamma z \cos \beta) \cos \beta \end{aligned}$$

$$\sigma_n = \gamma z \cos^2 \beta$$

$$\text{Shear stress } (\tau) = \gamma z \sin \beta \cdot \cos \beta$$

Let  $\tau_f$  be the shear strength of soil

$$\tau_f = c + \sigma_n \tan \phi$$

$$\tau_f = \sigma_n \tan \phi$$

$$\tau_f = \gamma z \cos^2 \beta \cdot \tan \phi$$

$$\text{Factor of safety} = \frac{\tau_f}{\tau} = \frac{\gamma z \cos^2 \beta \cdot \tan \phi}{\gamma z \cos \beta \cdot \sin \beta}$$

$$FOS = \frac{\tan \phi}{\tan \beta} = \frac{\tan 36}{\tan 30}$$

$$FOS = 1.258 > 1$$

Slope is safe.

P-2. A Vertical cut is made in a clay deposit having  $c = 30 \text{ kN/m}^2$  &  $\phi = 0$ ,  $\gamma = 16 \text{ kN/m}^3$ . Find the maximum height of the cut which can be temporarily supported.

Take for  $\phi = 0$ ,  $S_n = 0.261$ .

Sol  
~~Tab~~ Stability Number ( $S_n$ ) =  $\frac{c}{F_c \cdot \gamma \cdot H}$

For critical condition,  $F_c = 1$ .

$$S_n = \frac{c}{\gamma \cdot H_c}$$

$$0.261 = \frac{30}{16 \times H_c}$$

$$H_c = \frac{30}{16 \times 0.261}$$

$$H_c = 7.18 \text{ m}$$