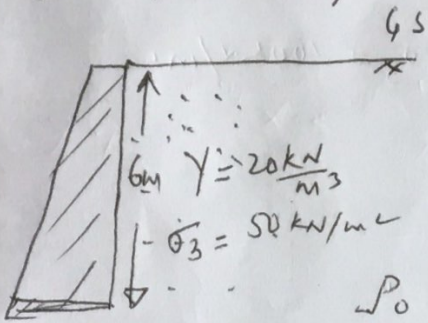


B.Tech 6th Semester (CIVIL ENGINEERING)

Instructor: RASHID MUSTAFA

Q-1 (120 kN/m)



$$\nu = \frac{\sigma_3}{\sigma_1 + \sigma_3} = \frac{50}{200} = \frac{1}{4} = 0.25$$

$$K_0 = \frac{\nu}{1 - \nu} = \frac{0.25}{0.75} = \frac{1}{3}$$

$$P_0 = \frac{1}{2} K_0 \gamma H^2 = \frac{1}{2} \times \frac{1}{3} \times 20 \times 36$$

$$P_0 = 120 \text{ kN/m}$$

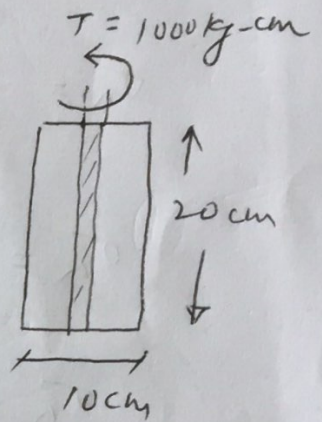
Q-2  $\left[ \frac{1}{\pi} \left( \frac{6}{7} \right) \right]$

$$S = \frac{T}{\pi D^2 \left( \frac{H}{2} + \frac{D}{6} \right)}$$

$$= \frac{10000}{\pi \times 100 \left( \frac{20}{2} + \frac{10}{6} \right)}$$

$$= \frac{10}{\pi \left( 10 + \frac{5}{3} \right)} = \frac{10 \times 3}{\pi \left( \frac{35}{2} \right)}$$

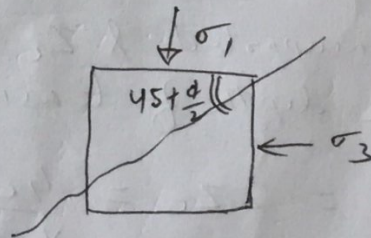
$$S = \frac{6}{7\pi} = \left[ \frac{1}{\pi} \left( \frac{6}{7} \right) \right] \text{ kg/cm}^2$$



Q-3 (40°)

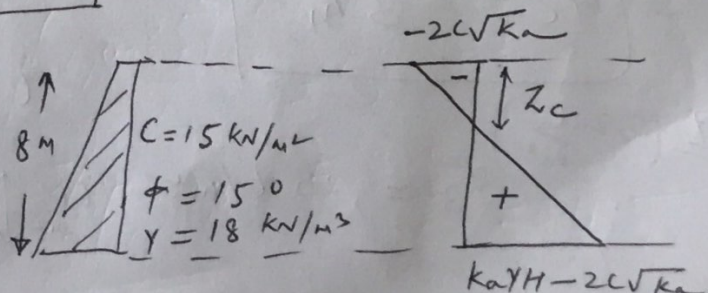
$$\alpha = 45 - \frac{\phi}{2}$$

$$\alpha = 45 - \frac{10}{2} = 40^\circ$$



Q-4 (-13.81 kN/m^2)

Active Pressure =  $-2c \sqrt{Ka}$

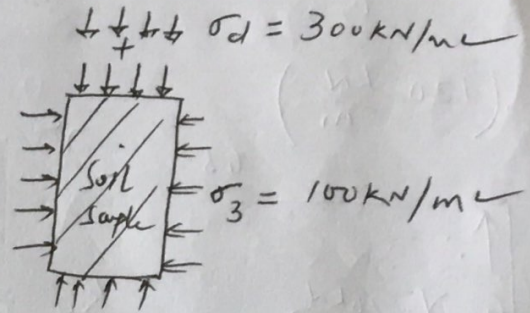


$$P_{a1 \text{ at top}} = -2 \times 15 \times \sqrt{\frac{1 - \sin 15}{1 + \sin 15}} = \boxed{-13.81 \frac{\text{kN}}{\text{m}^2}}$$

Q-5. (250  $\frac{\text{kN}}{\text{m}^2}$ )

$$\sigma_3 = 100 \text{ kN/m}^2$$

$$\begin{aligned} \sigma_1 &= \sigma_3 + \sigma_d \\ &= 400 \text{ kN/m}^2 \end{aligned}$$



Max<sup>m</sup> shear stress occur at 45°

$$\sigma_n = \sigma_1 \cos^2 \theta + \sigma_3 \sin^2 \theta + 2\tau_{xy} \sin \theta \cos \theta$$

OR

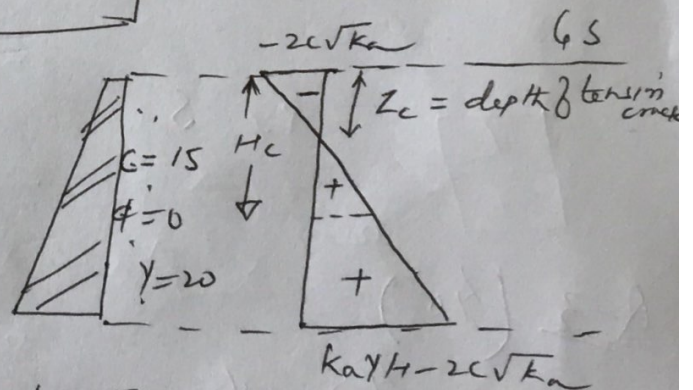
$$\sigma_n = \left( \frac{\sigma_1 + \sigma_3}{2} \right) + \left( \frac{\sigma_1 - \sigma_3}{2} \right) \cos 2\theta$$

$$\sigma_n = \left( \frac{400 + 100}{2} \right) + \left( \frac{400 - 100}{2} \right) \cos 90^\circ$$

$$\boxed{\sigma_n = 250 \text{ kN/m}^2}$$

Q-6 (3 m)

Let  $H_c$  be the height of unsupported &  $Z_c$  be the depth of tension crack

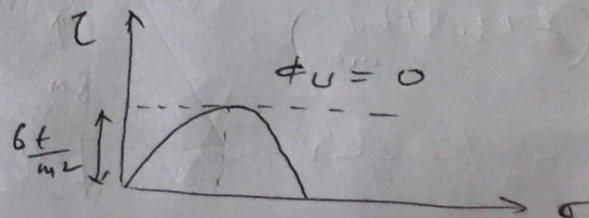


$$H_c = 2Z_c = \frac{4c}{\gamma \sqrt{K_a}} = \frac{4 \times 15}{20 \sqrt{1}}$$

$$\boxed{H_c = 3 \text{ m}}$$

Q-7 (32  $\frac{\text{t}}{\text{m}^2}$ )

$$\sigma_3 = 20 \text{ t/m}^2$$

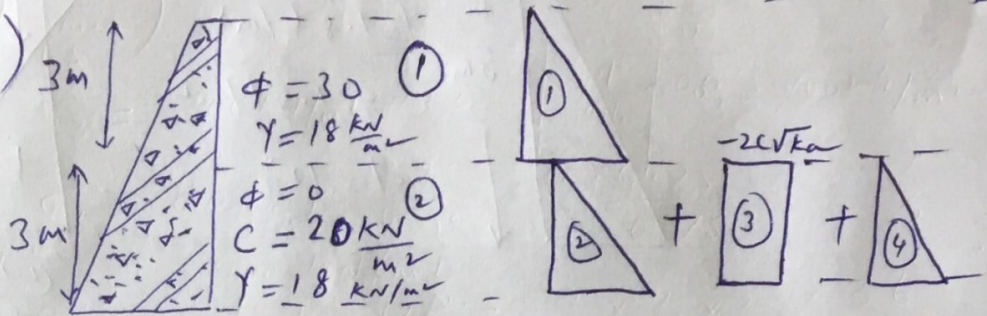


$$\sigma_1 = \sigma_3 \tan^2(45 + \frac{\phi}{2}) + 2c \tan(45 + \frac{\phi}{2})$$

$$\sigma_1 = 20 \tan^2(45) + 2 \times 6 \times \tan(45)$$

$$\sigma_1 = 20 \times 1 + 12 \times 1 = 32 \text{ t/m}^2$$

Q-8 (150 kN/m)



For Layer ①,  $K_{a1} = \frac{1 - \sin 30}{1 + \sin 30} = \frac{1}{3}$

For Layer ②,  $K_{a2} = \frac{1 - \sin 0}{1 + \sin 0} = 1$

$$P_a = P_{a1} + P_{a2} + P_{a3} + P_{a4}$$

$$= \frac{1}{2} \times \frac{1}{3} \times 18 \times 9 + \frac{1}{2} \times 1 \times 18 \times 9 - 2 \times 20 \times \sqrt{1} \times 3$$

$$+ 1 \times (18 \times 3) \times 3$$

$$= 27 + 81 - 120 + 162 = 150 \text{ kN/m}$$

Q-9 (0.467)

$$B = \frac{\Delta U}{\Delta \sigma_3} = \frac{70}{300 - 150} = \frac{70}{150}$$

$$B = 0.467$$

Q-10 (119.2 kPa)

$$c' = 20 \text{ kPa}$$

$$\phi' = 22^\circ$$

$$\sigma_3 = 150 \text{ kPa}, U = 100 \text{ kPa}$$

$$\sigma_3' = 150 - 100 = 50 \text{ kPa}$$

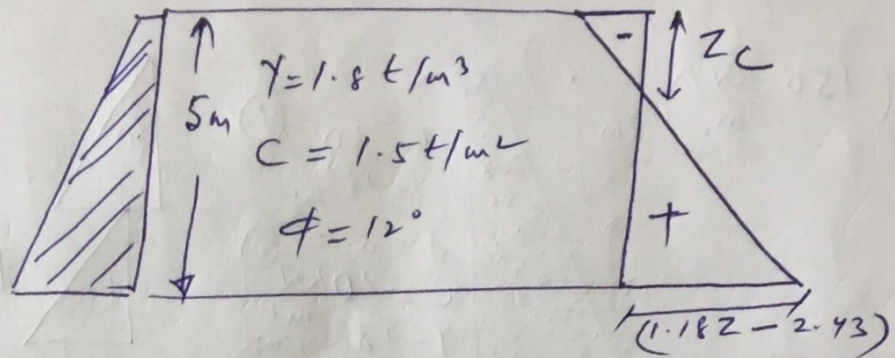
$$\sigma_1' = \sigma_3' \tan^2(45 + \frac{\phi'}{2}) + 2c' \tan(45 + \frac{\phi'}{2})$$

$$\sigma_1' = 50 \tan^2(45 + 11) + 40 \tan(56)$$

$$\sigma_1' = 169.20 \text{ kN/m}^2$$

$$\sigma_d = 169.2 - 50 = 119.2 \text{ kN/m}^2$$

Q-11 (5.1 t/m)



$$z_c = \frac{2c}{\gamma \sqrt{K_a}} = \frac{2 \times 1.5}{1.8 \times \sqrt{\frac{1 - \sin 12^\circ}{1 + \sin 12^\circ}}}$$

$$= 2.058 \text{ m}$$

$$K_a = \frac{1 - \sin 12^\circ}{1 + \sin 12^\circ}$$

$$= 0.656$$

$$p_a = K_a \gamma z - 2c \sqrt{K_a}$$

$$= 0.656 \times 1.8 z - 2 \times 1.5 \sqrt{0.656}$$

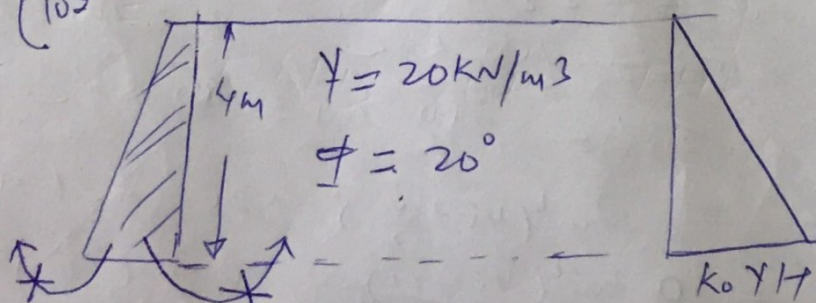
$$p_a = (1.18z - 2.43)$$

$$P_a = \int_{z_c}^H (p_a) dz$$

$$= \int_{2.058}^5 (1.18z - 2.43) dz$$

$$= 5.10 \text{ t/m}$$

Q-13 (105.28)

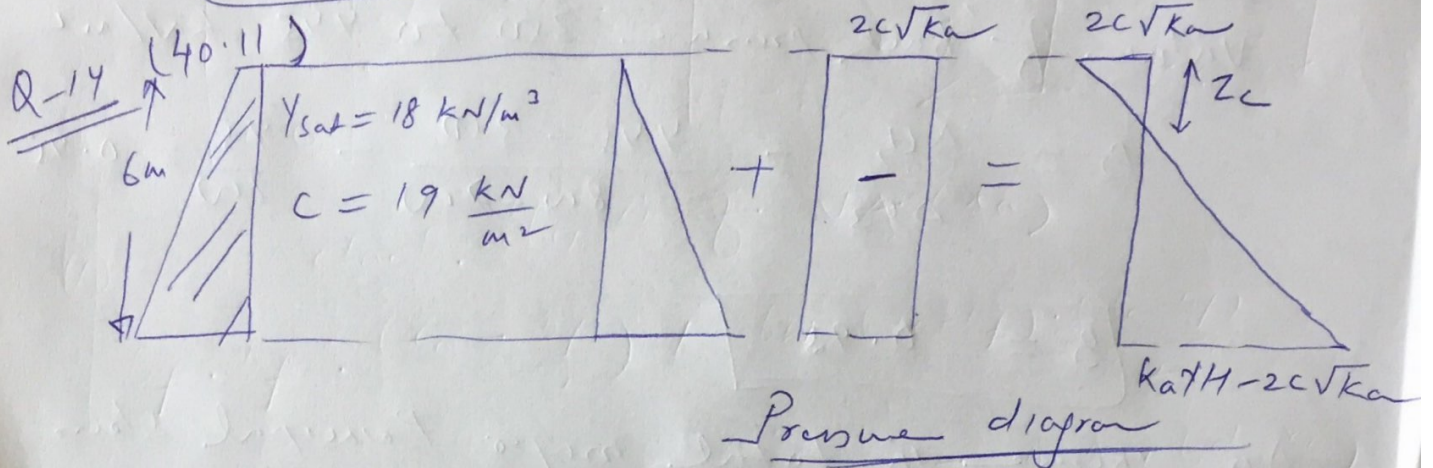


$$A_{\text{rest thrust}} (P_0) = \frac{1}{2} k_0 \gamma H^2$$

$$k_0 = 1 - \sin \phi = 1 - \sin 20^\circ = 0.658$$

$$P_0 = \frac{1}{2} \times 0.658 \times 20 \times 16 = 105.28 \text{ kN/m}$$

$$P_0 = 105.28 \text{ kN/m}$$



$$\text{depth of tension crack } (z_c) = \frac{2c}{\gamma\sqrt{k_a}} = \frac{2 \times 19}{7.8\sqrt{1}} = 2.11 \text{ m}$$

Pressure at depth (z)

$$P_a = k_a \gamma z - 2c\sqrt{k_a}$$

$$= 1 \times 18 \times z - 38\sqrt{1}$$

$$= (18z - 38)$$

Total active thrust before tension crack ( $P_a$ )

$$P_a = \int_0^H (k_a \gamma z - 2c\sqrt{k_a}) dz = \int_0^6 (18z - 38) dz$$

$$P_a = 96 \text{ kN/m}$$

Total active thrust after tension crack ( $P_a$ )

$$P_a = \int_{z_c}^H (k_a \gamma z - 2c\sqrt{k_a}) dz = \int_{2.11}^6 (18z - 38) dz$$

$$P_a = 136.11 \text{ kN/m}$$

$$\text{Difference} = (136.11 - 96) = 40.11 \text{ kN/m}$$

$$\underline{\underline{Q-15}} \quad (0.357, 0.95) \quad \sigma_3 = 700 \text{ kN/m}^2$$

For an increase in cell pressure from 700 to 800 kN/m<sup>2</sup>, the pore pressure increases from the value of back pressure 350 to 445 kN/m<sup>2</sup>

$$B = \frac{\Delta U_1}{\Delta \sigma_3} = \frac{445 - 350}{800 - 700} = \frac{95}{100} = 0.95$$

$$\boxed{B = 0.95}$$

An increase in total major principal stress from 800 kN/m<sup>2</sup> to (800 + 575) kN/m<sup>2</sup> produced a corresponding increase in PWP from 445 to 640 kN/m<sup>2</sup>

$$A' = \frac{\Delta U_2}{\Delta \sigma_1 - \Delta \sigma_3} = \frac{640 - 445}{575}$$

$$= \frac{195}{575} = 0.339$$

$$A' = AB$$
$$A = \frac{A'}{B} = \frac{0.339}{0.95} = 0.357$$

$$\boxed{A = 0.357}$$

END OF THE SOLUTION