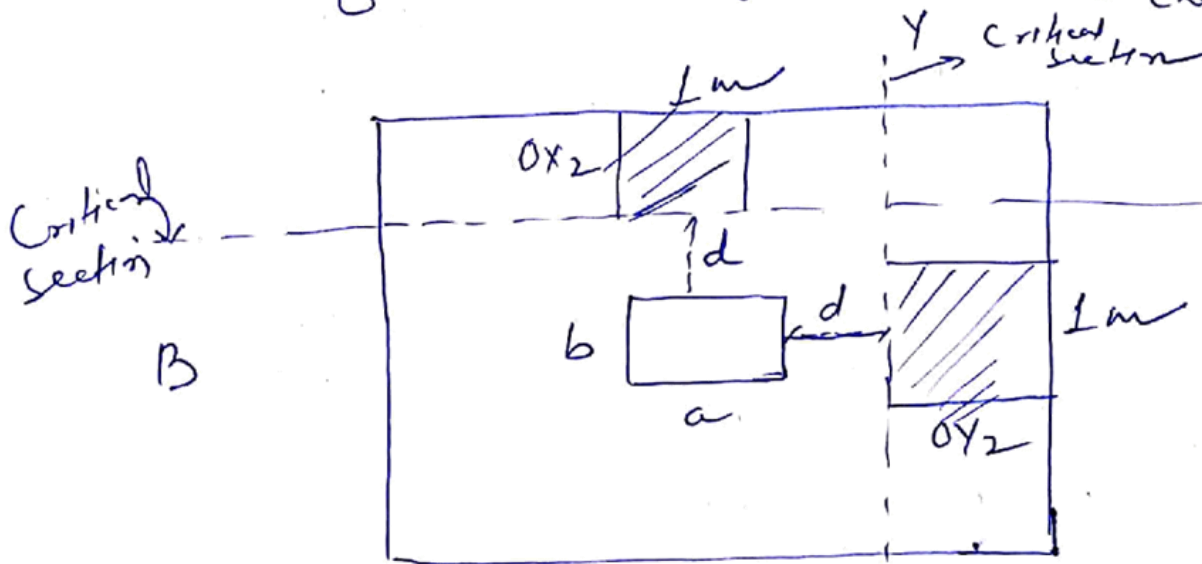


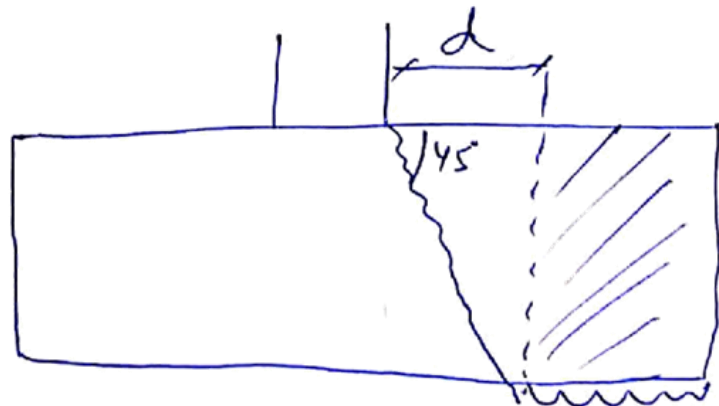
Department of Civil Engineering Katihar Engineering College, Katihar

Subject: Design of Concrete Structure-I
Topic: Footing
Lecture: 02
Course Instructor: Prof. Rashid Mustafa

② Check for One way shear (single shear check)



$$L \quad \left[\left(\frac{L-a}{2} \right) - d \right]$$



Critical section for SF (One way shear)

- At "d" distance from face of Column
- Most critical section will be the section where overhang is maximum.
- SF at x-x overhang is maximum

$$OY_2 = \left[\frac{L-a}{2} - d \right]$$

Total shear force for 1m strip

$$V_y = w_o \times L \times OY_2$$

$$V_y = w_o \times L \times \left[\left(\frac{L-a}{2} \right) - d \right]$$

↳ WSM

$$V_y = w_{ud} \times L \times \left[\frac{L-a}{2} - d \right]$$

↳ LSM

Nominal shear stress

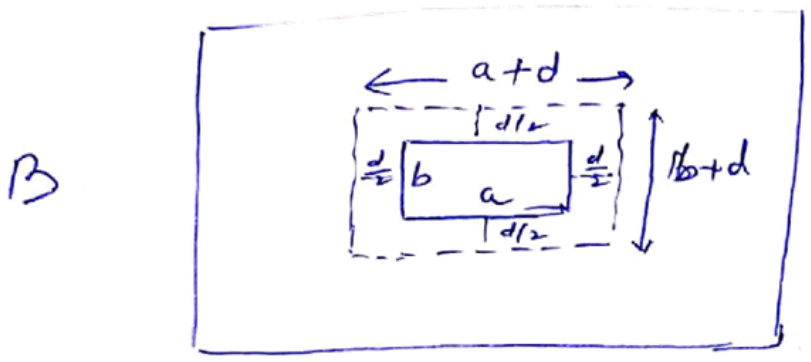
$$\tau_v = \frac{V}{B \cdot d} = \frac{V}{1000 \times d} \leq k \cdot \tau_c$$

$$\tau_{vu} = \frac{V_u}{B \cdot d} = \frac{V_u}{1000 \times d} \leq k \cdot \tau_c$$

Value of k

Slab thickness (mm)	≤ 150	175	200	225	250	275	≥ 300
k	1.30	1.25	1.20	1.15	1.10	1.05	1.00

4 Check for Punching Shear (Two way shear)



↳ Critical section is at " $\frac{d}{2}$ " distance all around the column section.

Net Punching force = $P - W_o(a+d)(b+d)$
 (P_{net})

↳ Punching shear stress (τ_{vp}) = $\frac{P_{net}}{\text{Resisting Area}}$
 = $\frac{P_{net}}{\text{Perimeter} \times \text{width}}$

$$\tau_{vp(\text{developed})} = \frac{P - W_o(a+d)(b+d)}{2[(a+d)+(b+d)] \times d}$$

↳ WSM

In LSM

$$\tau_{vp(\text{dev})} = \frac{P_u - W_{uox}(a+d)(b+d)}{2[(a+d)+(b+d)] \times d}$$

→ Permissible Punching shear stress

$$\tau_{vp(\text{Permissible})} = k_{\beta} \times 0.16 \sqrt{f_{ck}}$$

↳ WSM

$$\tau_{vp(\text{Permissible})} = k_{\beta} \times 0.25 \sqrt{f_{ck}}$$

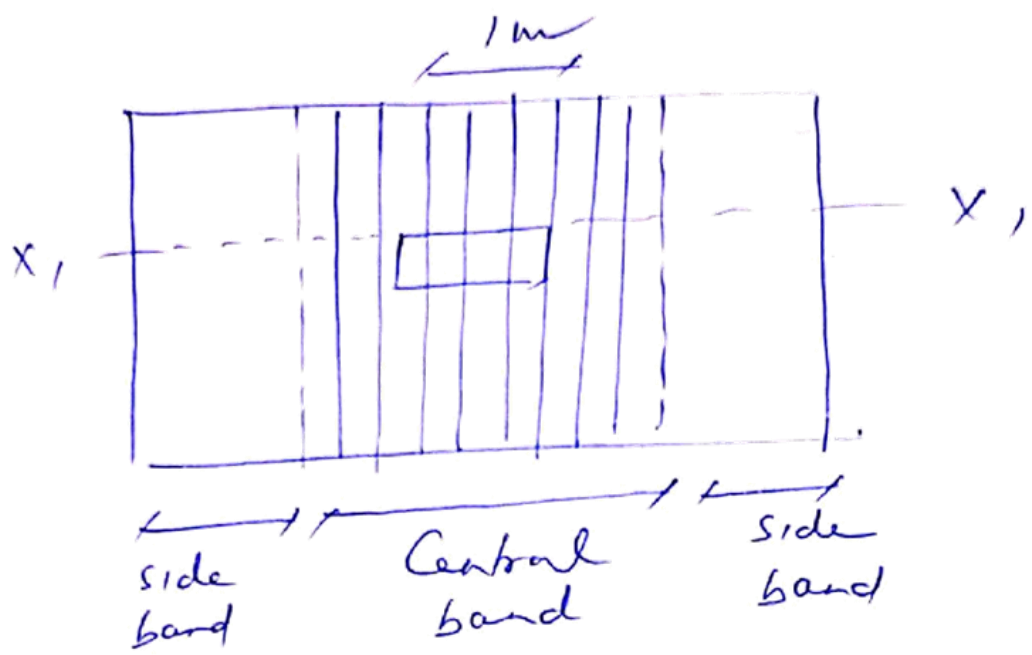
↳ LSM

When, $k_{\beta} = \left(0.5 + \frac{b}{a}\right) \neq 1.0$

Steps . Area of steel .

(a)

For Moment about x-x (for M_x)



Design of shorree bars .

Area of steel required for M_x (for L_m width)

$$A_{st} = \frac{BM}{\sigma_{st} \cdot J \cdot d} \rightarrow WSM$$

$$A_{st} = \frac{BM_u}{0.87 f_y J \cdot d} \rightarrow LSM$$

$$A_{st} = \frac{0.5 f_{ck}}{f_y} \left[1 - \sqrt{1 - \frac{4.6 M_u}{f_{ck} B_1 d^2}} \right] B_1 d$$

$B_1 = 1000 \text{ mm}$

→ Area of steel required for full width (L) = $L \times A_{st}$

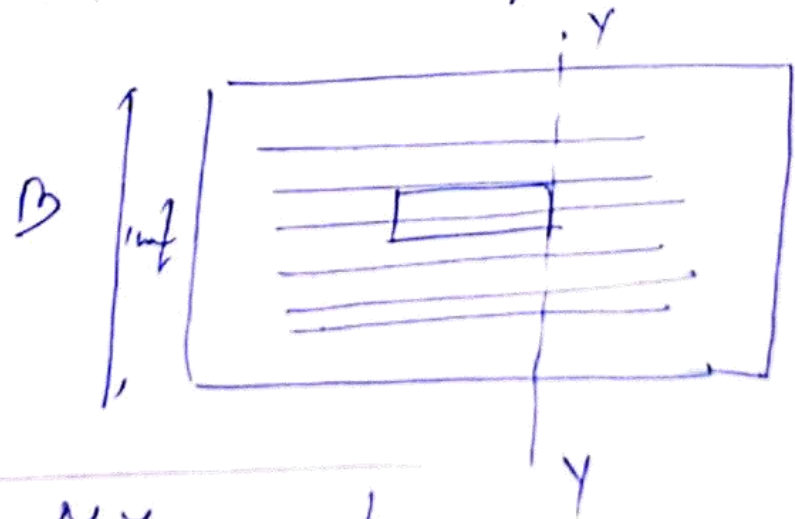
→ Total No of bars for full width (n_T) = $\frac{L \times A_{st}}{\frac{\pi}{4} \times \phi^2}$

→ No of reinforcement to be provided in central band (n_c) = $n_T \times \frac{2}{(1 + \frac{L}{B})}$

→ No of reinforcement to be provided on two side bands

$$(n_s) = \frac{n_T - n_c}{2}$$

(b) For Moment about Y-Y (For M_y)



$$A_{st} = \frac{M_y}{\sigma_{st} \cdot J \cdot d}$$

↳ use n_y

$$A_{st} = \frac{M_{uy}}{0.87 f_y J \cdot d}$$

For total width B total reinforcement = $B \times A_{st}$.

$$\text{Total No of bars } (n) = \frac{B \times A_{st}}{\frac{\pi}{4} \times \phi^2}$$

↳ distribute equally over full width B